Impact of hydrodynamic transport on Granular Activated Sludge: micro and macro scale investigations





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MOTIVATION

WASTEWATER TREATMENT











BIOFLOW





GAS AND CAS

 Conventional Activated Sludge (CAS) and Granular Activated Sludge (GAS)

CAS

GAS



ADVANTAGES OF GAS

- Spherical and strong microbial structure
- Good settling ability
- High density 1.05 g/ml
- Dimension up to 5 mm
- Aerobic granulation as a recent innovation in biological wastewater treatment

/Morgenroth et al. (1997), Peng et al. (1999), Buen et al.(1999), Etterer and Wilderer (2001), Tay et al. (2001)/

GAS DEFINITION

Granules making up aerobic granular activated sludge are to be understood as aggregates of microbial origin, which do not coagulate under reduced hydrodynamic shear, and which settle significantly faster than activated sludge flocs

(1st IWA Workshop of Aerobic Granular Sludge, TU München, 2004)

GRANULES FORMATION



GAS AND SBR

Main factors influencing granules structure and formation

Superficial Gas Velocity (SGV)
/van Loosdrecht et al. (1995), Tay et al. (2001), Zima et al. (2007)/

 Substrate type and concentration of synthetic wastewater food /Zhu et al. (2001), Etterer and Wilderer (2001)/

 Extracellular Polymeric Substances (EPS) /Oashi and Harada (1994), Tay et al.(2001)/

Optimal bioreactor configuration

/Beun et al. (1999), Liu and Tay (2002), Zima-Kulisiewicz et al. (2008)/

Mechanical forces /Zima et al. (2007)/



EXPERIMENTAL SETUP



SBR PROCESS



- Compact structure of granules an high biomass concentration
- Good settling ability, no settling tank

OPTICAL IN-SITU TECHNIQUES

He-Ne laser



OPTICAL IN-SITU TECHNIQUES

micro Particle Image Velocimetry

Microscope Carl Zeiss Axiotech 100

High speed CCD camera Mikrotron Resolution of images 860x1024

PIV Software PIVview 3C Cross correlation mode Interrogation window size 32x32 pixels Grid size 20x20 pixels

Post processing with TECPLOT



BIOCOMPATIBLE OPTICAL IN-SITU TECHNIQUES

Appropriate tracer particles + suitable illumination

- Artificial tracers are rejected
- Biocompatible tracer particles





DIMENSIONLESS REPRESENTATION OF THE RESULTS

Time	$t = \frac{\underline{t}}{t_s}$	Forces	$\vec{F}_i = \frac{\vec{F}_i}{\vec{F}_G}$
Liquid velocity	$u_w = \frac{u_w}{SGV}$	Liquid velocity	$u = \frac{\underline{u}}{u_{max}}$
Liquid velocity components	$u_w = \frac{u_w}{SGV}$ $v_w = \frac{v_w}{SGV}$	X axis	X D
Shear strain rate	$\dot{\gamma} = rac{\dot{\gamma}}{\dot{\gamma}_{max}}$	Y axis	Y H _{max}
Normal strain rate	$\dot{\varepsilon} = \frac{\dot{\underline{\varepsilon}}}{\dot{\varepsilon}_{max}}$	Z axis	Z D

OBSERVABLE FLUID FLOW PATTERNS



DIMENSIONLESS FLUID VELOCITY increasing tendency with height in SBR

NON-STATIONARITY OF THE FLOW



INFLUENCE OF WASTING





without wasting

with wasting

INFLUENCE OF WASTING



INFLUENCE OF WASTING





DIMENSIONLESS NORMAL STRAIN RATE



Z/D = 0.11

DIMENSIONLESS SHEAR STRAIN RATE



Z/D = 0.09

Z/D = 0.11

FLUID DYNAMIC FORCES



Drag force	$\underline{\vec{F}_{D}} = C_{D}A_{p}\frac{\rho_{W}}{2}\left \vec{u}_{W} - \vec{u}_{P}\right \left(\vec{u}_{W} - \vec{u}_{P}\right)$	$\vec{F}_{D} = 1.31 \times 10^{-1}$
Basset force	$\underline{\vec{F}_{B}} = \frac{3}{2} D_{P}^{2} \sqrt{\pi \rho_{W} \mu_{W}} \left[\int_{0}^{t} \frac{\frac{d}{dt} (\vec{u}_{W} - \vec{u}_{P})}{\sqrt{t - t'}} dt' + \frac{(\vec{u}_{W} - \vec{u}_{P})_{0}}{\sqrt{t}} \right]$	$\vec{F}_{B} = 2.42 \times 10^{-3}$
Added mass force	$\vec{\underline{F}}_{A} = \frac{1}{2} C_{A} \rho_{W} \frac{m_{P}}{\rho_{P}} \frac{d}{dt} (\vec{u}_{W} - \vec{u}_{P})$	$\vec{F}_{A} = 2.74 \times 10^{-3}$
Saffman force	$\underline{\vec{F}_{S}} = 1.61 D_{P}^{2} \sqrt{\rho_{W} \mu_{W}} \frac{1}{\left \vec{\omega}_{W}\right } \left[\left(\vec{u}_{W} - \vec{u}_{P}\right) \times \vec{\omega}_{W} \right]$	$\vec{F}_{S} = 7.17 \times 10^{-2}$
Magnus force	$\underline{\vec{F}_{M}} = C_{LR} A_{P} \frac{\rho_{W}}{2} \vec{u}_{W} - \vec{u}_{P} \frac{\vec{\Omega} \times (\vec{u}_{W} - \vec{u}_{P})}{ \vec{\Omega} }$	$\vec{F}_{M} = 2.43 \times 10^{-2}$
Lift rotational force	$\vec{\underline{T}}_{R} = \frac{\rho_{W}}{2} \left(\frac{D_{P}}{2}\right)^{5} C_{R} \left \vec{\Omega}\right \vec{\Omega}$	$\vec{T}_{R} = 5.86 \times 10^{-3}$

MICROSCOPIC ANALYSIS

3 bioreactors with the same working volume, the same geometrical configuration and different flow rate



influence of mechanical forces not only depends on the load magnitude but also on duration of the process /Esterl et al. (2002), Zima et al. (2007)/

FATIGUE EFFECT

MICROSCOPIC ANALYSIS

HYDRODYNAMIC SELECTION OF MICROORGANISMS



BIG DIVERSITY OF MICROORGANISMS UNDER DIFFERENT FLOW RATES

/Zima et al. (2007)/

MICROORGANISMIC FLOW



CHARACTERISTIC FLOW PATTERN



DIFFERENT SEEDING PARTICLES

Yeast cells 3-10 µm

Milk 0.3-3 µm





VELOCITY



u_{max}= 0.20



CONVECTIVE KINETIC ENERGY

one ciliate

colony



synergy factor 1.7

NORMAL STRAIN RATE



synergy factor 3.3

SHEAR STRAIN RATE

one ciliate



synergy factor 2.7

VELOCITY

1:1





1:4

u_{max}= 0.17

CONVECTIVE KINETIC ENERGY

1:1

1:4



synergy factor 30

NORMAL STRAIN RATE

1:1

1:4



synergy factor 3.8



1:1

1:4



synergy factor 5

CONCLUSIONS

- ✓ characteristic flow pattern in SBR (micro and macro scale)
- ✓ big influence of granules on the flow pattern
- ✓ granulation only under appropriate flow conditions
- ✓ normal and shear strain rates significant effect on granules formation
- ✓ buoyancy, drag, collisional, lift forces crucial role in SBR
- different flow conditions biomechanical fatigue effect, hydrodynamic selections of microorganisms
- ✓ ciliates important role for granules formation
- ✓ flow induced by ciliates efficient way for nutrient transport with minimum energy requirement
- ✓ efficient cooperative colony work